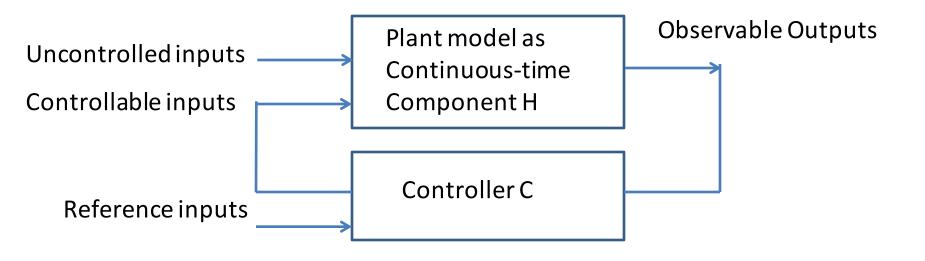
CS:4980 Foundations of Embedded Systems

Dynamical Systems Part IV

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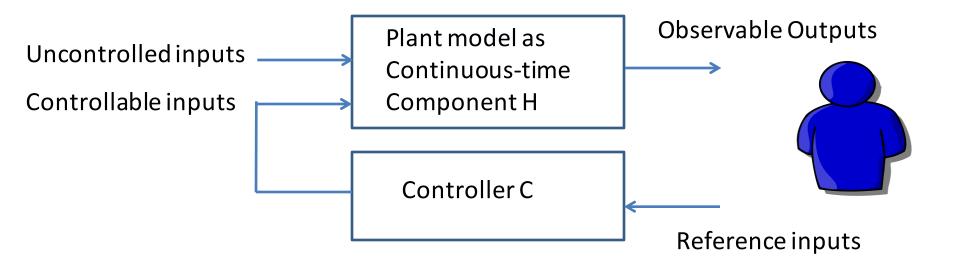
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Control Design Problem



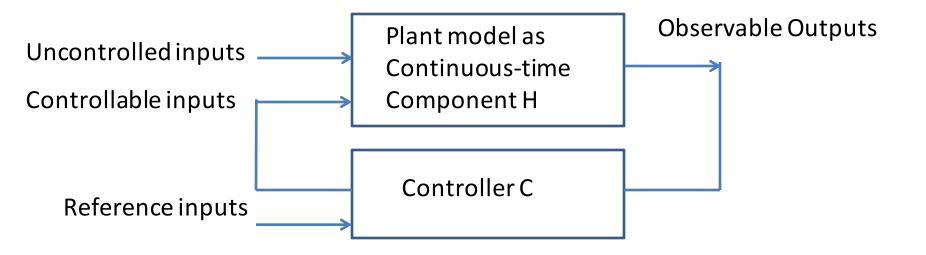
- ☐ Design a controller C so that the composed system C || H is stable
- Reference inputs are high-level commands supplied by humans (e.g. desired speed of the car, temperature in the room)
- ☐ Controller should satisfy additional safety/liveness requirements corresponding to reference inputs (e.g. speed of car eventually becomes close to desired cruising speed)

Open Loop Controller



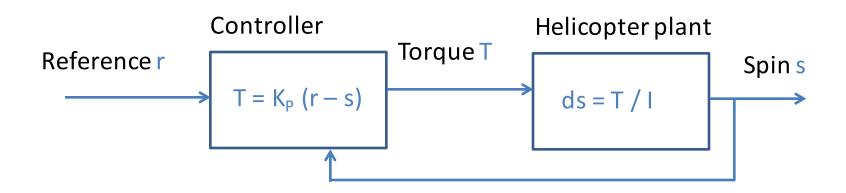
- ☐ Plant outputs not fed to the controller
 - Benefit: Sensors not needed (less expensive)
- ☐ Controller simply maps reference inputs to controllable inputs
 - Knowledge of plant dynamics hard-coded in this algorithm
- ☐ Human intervention typically necessary to maintain acceptable performance

Feedback Controller



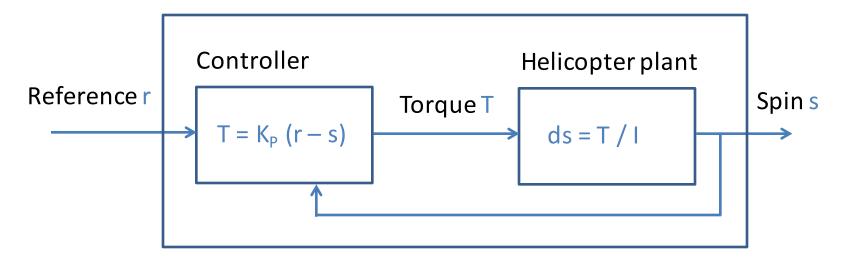
- ☐ Controller adjusts controllable inputs in response to outputs
 - Can respond better to variations in disturbances
 - Performance depends on how well outputs can be measured
- ☐ Two control design techniques:
 - 1. Mathematical, based on theory of linear systems
 - 2. PID controllers, widely used in practice

Feedback Controller for Helicopter Model



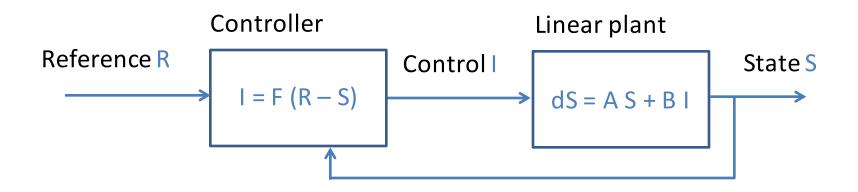
- Design controller so that composed system is stable
- \square Error e = (r s): difference in desired value and observed output
- lue Proportional controller: output ${\sf T}$ is proportional to error ${\sf e}$
- ☐ Constant K_p: *proportional gain*
- ☐ Note: the direction of torque changes with sign of the error

Stabilizing Controller for Helicopter Model



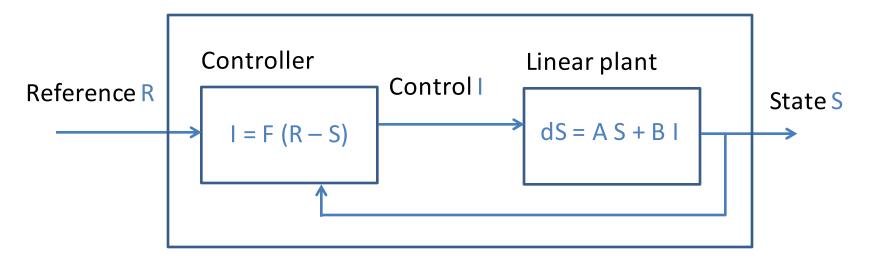
- \Box Dynamics of the composed system: $ds/dt = K_p (r s) / I$
- ☐ When is this system asymptotically stable? BIBO stable?
 - When the coefficient $-K_p/I$ is negative
- ☐ Control design: choose a positive *gain constant* K_p
 - Rate of convergence depends on magnitude of K_P

Feedback Controller for Linear Systems



- ☐ Assume the controller observes the complete state vector S
- Reference signal R has same dimension as state vector S
- ☐ State feedback controller: linear transformation
- \square Matrix F: gain matrix of dimension m × n, with m = |||, n = |S||

Stabilization by Linear State Feedback



☐ Dynamics of the composed system:

$$dS/dt = (A - B F) S + B F R$$

- ☐ Goal of control design: define the gain matrix F so that the composed system is asymptotically, and so BIBO, stable
 - Given matrices A and B, find F such that each eigenvalue of A – B F has negative real part

Design of Gain Matrix

- \square System dynamics: dS/dt = AS + BI with n state and m input vars
- ☐ Design goal: given matrices A and B, find F such that each eigenvalue of A B F has negative real part
- ☐ When is this possible?
- \square Suppose we choose desired eigenvalues λ_1 , ..., λ_n and solve the system of equations

$$det(A - B F - \lambda I) = (\lambda - \lambda_1) (\lambda - \lambda_2) ... (\lambda - \lambda_n)$$

where the $m \times n$ entries of matrix F are the unknowns

- ☐ When is this system guaranteed to be solvable?
- ☐ Does the existence of a solution depend on the choice of eigenvalues?

Controllability

☐ Given an n×n matrix A and n×m matrix B, consider the controllability n×mn matrix

$$C[A,B] = (B AB A^2B ... A^{n-1}B)$$

m columns of B followed by m columns of A B, then of A A B, ...

- ☐ Recall: the *rank* of a matrix is the maximum number of linearly independent rows
- \Box The matrix pair (A, B) is *controllable* if C[A,B] has rank n

Theorem: The following are equivalent:

- 1. The matrix pair (A, B) is controllable
- 2. For any set $\{\lambda_1, ..., \lambda_n\}$ of complex numbers such that a + bj is in the set iff its conjugate a bj is in the set, there is a $n \times m$ gain matrix F such that the eigenvalues of A B F are $\lambda_1, ..., \lambda_n$

Example: Controllability test

Consider 2-dimensional system with one input u, with dynamics given by

$$d s_1 = 4 s_1 + 6 s_2 + 2 u$$

 $d s_2 = s_1 + 3 s_2 + u$

- What are the matrices A, B, C[A, B]?
- What is the rank of C[A, B]?

Advantages of Controllability

☐ Consider a linear system with dynamics:

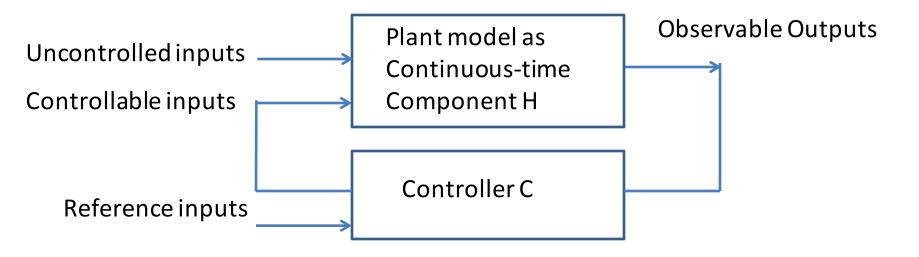
$$dS/dt = AS + BI$$
; initial state s_0

- ☐ Suppose (A, B) is controllable
- Then, for every system state s there is an input signal I and a time t_g such that

$$S(t_g) = s$$

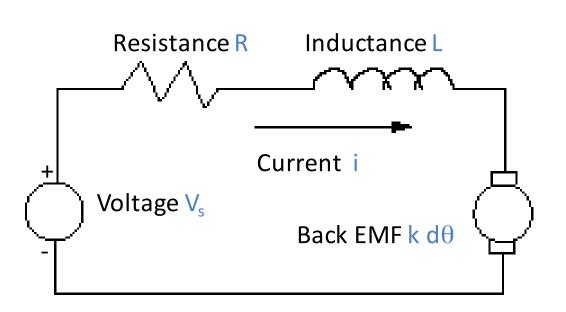
where S is the unique response signal for I and S₀

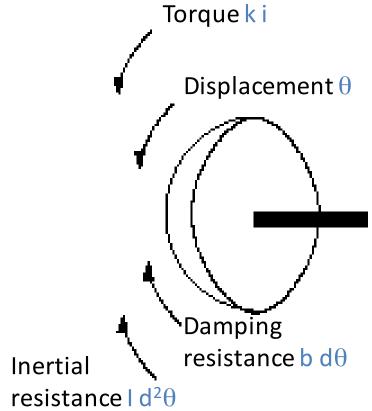
PID Controllers



- ☐ Strategy for designing controllers that is widely used in practice
- ☐ Error = Reference Inputs Observable Outputs
- ☐ Controller's output is sum of 3 terms:
 - Term proportional to error
 - Integral term to handle cumulative error
 - Derivative term in response to rate of change of error

DC Motor





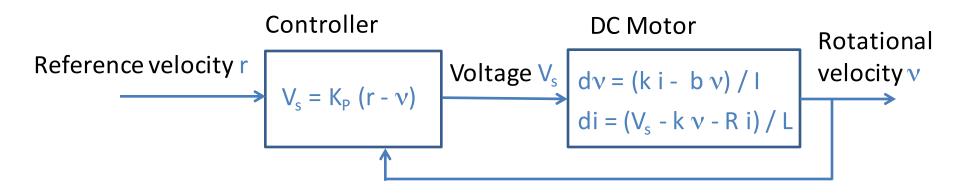
Laws of electrical circuits:

$$L di/dt + R i + k d\theta/dt = V_s$$

Laws of motion for the shaft:

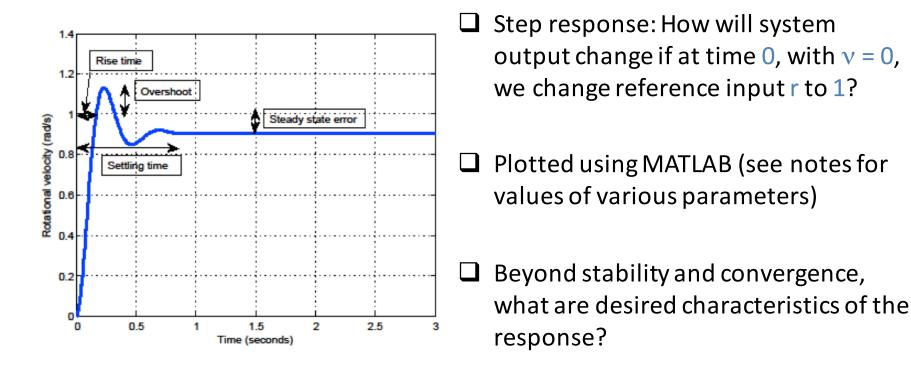
$$I d^2\theta/dt^2 + b d\theta/dt = k i$$

Proportional Controller for DC Motor

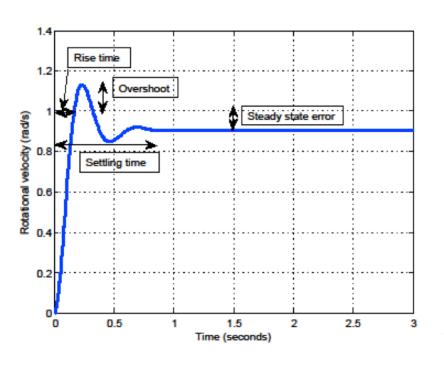


- ☐ DC Motor modeled as a linear system with 2 state variables, 1 input variable, and 1 output variable
- \Box Feedback controller observes rotational velocity \mathbf{v} , and adjusts voltage to make \mathbf{v} equal to desired velocity \mathbf{r}
- First attempt: proportional controller (P controller)

Step Response of P Controller

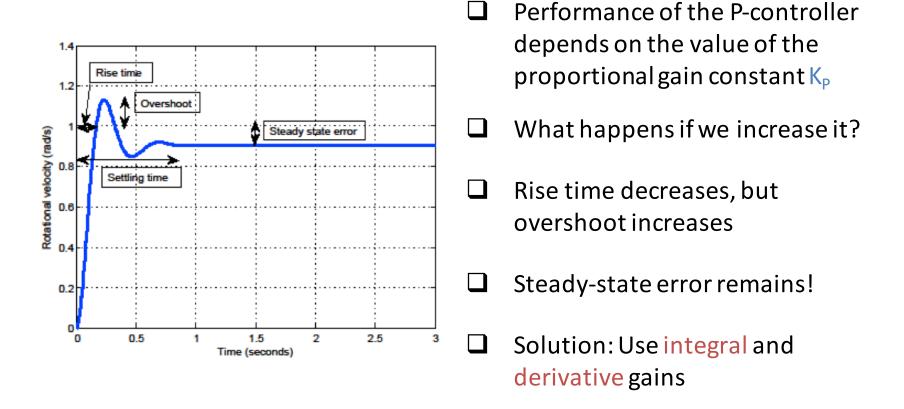


Characteristics of the Step Response

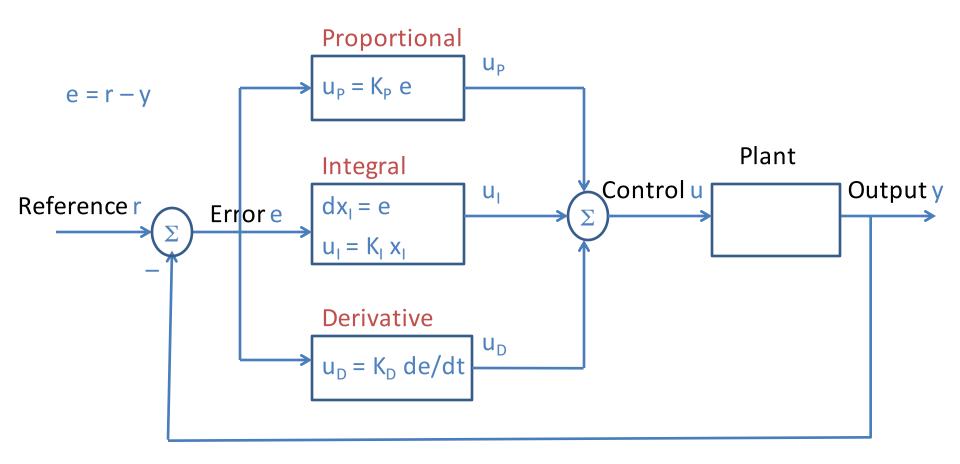


- Overshoot: Difference between maximum output value and reference value (12% in this plot)
- Rise Time: Time at which the output value crosses reference value (0.15sec in this plot)
- 3. Settling Time: Time at which output value reaches steady-state value (0.8sec in this plot)
- 4. Steady State Error: Difference between steady-state output value and reference (10% in this plot)

Improving the Step Response



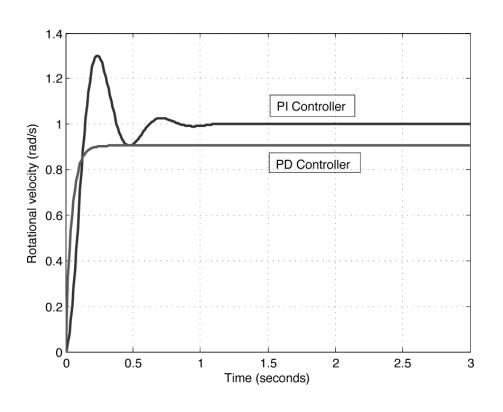
Generic PID Controller



PID Controller

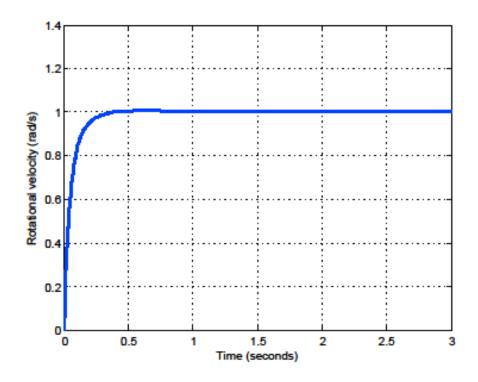
- ☐ If e(t) is the error signal, then the output u(t) of the PID controller is sum of 3 terms:
 - Proportional term: $K_P e(t)$, where K_P is the *proportional gain* (response to current error)
 - Integral term: $K_i \int_0^t \mathbf{e}(t) dt$, where K_i is the *integral gain* (response to error accumulated so far)
 - Derivative term: K_D (d/dt)e(t), where K_D is the *derivative gain* (response to current rate of change of error)
- ☐ Special cases of controllers: P, PD, PI

PI and PD Controllers for DC Motor



- PI Controller: adding integral term to proportional controller gets rid of steady state error
 - Overshoot, rise time, setting time increase (why?)
- PD controller: adding derivative term to proportional controller gets rid of overshoot
 - Steady state error remains

PID Controller for DC Motor

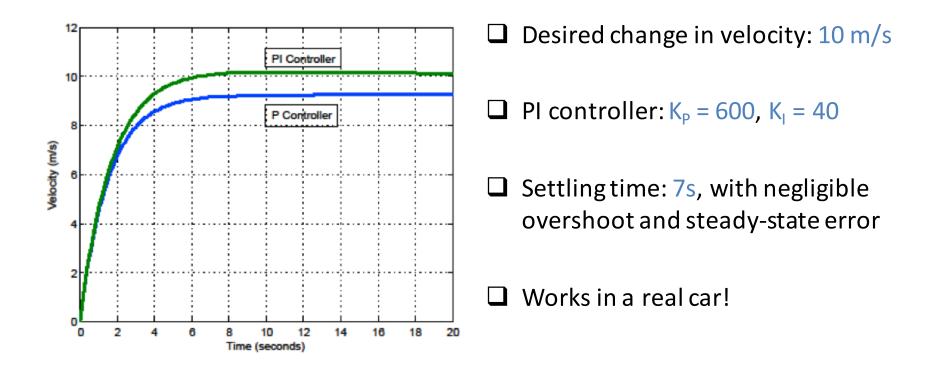


Excellent performance on all metrics: $K_p = 100$, $K_D = 10$, $K_I = 200$ Small rise time, settling time, negligible steady state error, no overshoot

Designing PID Controllers

- \Box What are the effects of changing the gain constants K_P , K_D , K_I ?
- ☐ Broad co-relationships well understood
- Control toolboxes allow automatic tuning of parameters
- ☐ PID controllers seem to work well even when the actual system differs significantly from the plant model
 - Computation of control output depends only on the measured error, and not on the model!

PI Cruise Controller



Credits

Notes based on Chapter 6 of

Principles of Cyber-Physical Systems

by Rajeev Alur MIT Press, 2015